This application note is a reference describing recommended noise suppression parts and board layouts that help reduce conductive noise and emission noise for the S-19932/19933 Series. It also summarizes CISPR25 compliant measurement results.

Refer to the datasheets of the S-19932/19933 Series for details and specs.
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1. Need for Noise Suppression Parts

Figure 1 shows the results of a voltage method measurement of a circuit to which no noise suppression parts have been applied. Although the measurement results significantly exceeded the CISPR25 class 5 specifications, this is not limited to the S-19932/19933 Series as general switching regulator ICs exhibit the similar tendency. For this reason, noise suppression parts must be applied to allow the IC to meet the stringent CISPR25 class 5 requirements.

![Figure 1](image1.png)

S-19933A (2.2 MHz), \(V_{IN} = 13\) V, \(V_{OUT} = 5\) V, \(I_{OUT} = 600\) mA, without noise suppression parts

Figure 2 is a circuit diagram to which the recommended noise suppression parts \(L_2\), \(C_{F2}\), and \(C_{F4}\) listed in Table 1 have been added. Figure 3 shows the results of a voltage method measurement carried out on this circuit. The addition of noise suppression parts reduces noise by as much as 20 MHz or more allowing the IC to meet CISPR25 class 5 requirements. Also, the S-19932/19933 Series optimally adjusts the SW pin slew rate in the IC so that the minimum of noise suppression parts will obtain a substantial margin.

![Figure 2](image2.png)

![Figure 3](image3.png)

*1. Noise suppression parts

<table>
<thead>
<tr>
<th>Parts</th>
<th>Name</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>(C_{F2})</td>
<td>4.7 (\mu)F</td>
</tr>
<tr>
<td></td>
<td>(L_2)</td>
<td>4.7 (\mu)H</td>
</tr>
<tr>
<td></td>
<td>(C_{F4})</td>
<td>4.7 (\mu)F</td>
</tr>
</tbody>
</table>

Table 1

S-19933A (2.2 MHz), \(V_{IN} = 13\) V, \(V_{OUT} = 5\) V, \(I_{OUT} = 600\) mA, with noise suppression parts
2. **Board Layout**

2.1 **Placement of input capacitors (C\text{IN0}, C\text{IN1}) and VIN and VSS layouts**

The placement of input capacitors and VIN and VSS wirings are crucial. The input capacitors are of paramount importance and should be placed as close to the IC as possible and on the same surface layer. C\text{IN1} is an essential capacitor to ensure stable IC operation and to suppress noise. C\text{IN0} is a capacitor of approximately 0.1 $\mu$F which is connected in parallel to C\text{IN1}. Add this capacitor as required to suppress mainly 10 MHz or larger noise. **Figure 4** shows an example of placing input capacitors in the immediate vicinity of the IC. The bold line indicates the current path the instant the high side power MOS FET in the IC turns on. First, current flows from the input capacitors to the VIN pin. Next, the current goes through the high side power MOS FET which is ON and the parasitic capacitance of low side power MOS FET which is OFF, both of which are inside the IC, in turn. Finally, the current returns to the input capacitors from the VSS pin. In this example, the reduction of impedance in the current path minimizes the noise generated in VIN and VSS wirings.

By contrast, **Figure 5** shows an example of input capacitors placed away from the IC and where the VSS pin is not connected to the VSS directly below the IC. At this time, there is a parasitic capacitance ($L_{p1}$) between the input capacitors and the VIN pin. In addition, as the current path between the input capacitors and the VSS pin is significantly extended, the parasitic capacitances ($L_{p2} + L_{p3} + L_{p4}$) extremely become large. In this example, impedance in the current path is increased and the noise generated in VIN and VSS wirings become larger.

![Good example vs Bad example](image)

2.2 **Placement and layout of Inductor (L1)**

The wiring area of the SW pin should be minimized. Reduce the wiring length within the allowable current capacity range. The rectangular wave voltage output from the SW pin contains high-frequency components, which could cause SW wiring to act as an antenna and thereby increase emission noise. In addition, as the high-frequency components in the rectangular wave voltage previously mentioned are transmitted from the SW pin to VOUT via the parasitic capacitance, SW wiring must be kept apart from VOUT wiring. Select a closed magnetic path inductor with low emission noise.

**Figure 6** shows an example where the wiring area between the SW pin and L1 is reduced and the distance between SW wiring and VOUT wiring is extended.

By contrast, **Figure 7** shows an example where the SW wiring area is excessively large, the distance between SW wiring and VOUT wiring is short, and the parasitic capacitance ($C_{p}$) is large.

![Good example vs Bad example](image)
2.3 Placement and layout of output capacitor (COUT1)

Place COUT1 close to the IC.

If the area of the current path indicated by the bold line (SW pin \( \rightarrow \) L1 \( \rightarrow \) COUT1 \( \rightarrow \) VSS pin) is reduced, the emission noise to be generated will be minimized.

Be sure to pull out VOUT wiring after routing through the COUT1 land. If this is not the case, smoothing due to L1 and COUT1 is weakened causing high-frequency components in the rectangular wave voltage of SW pin to be conducted to VOUT. Similarly, when increasing the line width, pull out a wiring after routing through COUT1 land.

Figure 8 is an example where the current path area is narrowed. VOUT wiring is pulled out after routing through the COUT1 land.

By contrast, Figure 9 is an example where the distance between the IC and COUT1 is long and the current path area is large. VOUT wiring is pulled out from L1 land without routing through COUT1 land.

Figure 10 is an example where VOUT line width is excessively increased before routing through COUT1 land.

2.4 Recommended board layout

Figure 11 shows the recommended board layout that reflects the explanations previously mentioned.
3. Measurement Conditions and Measurement Results

3.1 Measurement condition 1

Figure 12 shows a circuit diagram of S-19933A Evaluation Board. The parts listed in Table 2 are mounted.

*S-19933A (2.2 MHz), V_IN = 13 V, V_OUT = 5 V, I_OUT = 600 mA,
Compliant with CISPR25 Edition 4.0 2016-10

*1. Noise suppression parts

![Circuit Diagram of S-19933A Evaluation Board](image)

**Table 2**

<table>
<thead>
<tr>
<th>Symbol</th>
<th>Value</th>
<th>Part Number</th>
<th>Manufacturer</th>
</tr>
</thead>
<tbody>
<tr>
<td>CF2</td>
<td>4.7 μF</td>
<td>CGA4J1X7R1H475K125AC</td>
<td>TDK Corporation</td>
</tr>
<tr>
<td>L2</td>
<td>4.7 μH</td>
<td>TFM252012ALVA4R7MTAA</td>
<td>TDK Corporation</td>
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<tr>
<td>CF4</td>
<td>4.7 μF</td>
<td>CGA4J1X7R1H475K125AC</td>
<td>TDK Corporation</td>
</tr>
<tr>
<td>CIN1</td>
<td>4.7 μF</td>
<td>CGA4J1X7R1H475K125AC</td>
<td>TDK Corporation</td>
</tr>
<tr>
<td>CIN0</td>
<td>0.1 μF</td>
<td>CGA3E2X7R1H104K</td>
<td>TDK Corporation</td>
</tr>
<tr>
<td>L1</td>
<td>4.7 μH</td>
<td>TFM252012ALVA4R7MTAA</td>
<td>TDK Corporation</td>
</tr>
<tr>
<td>CREG1</td>
<td>1.0 μF</td>
<td>CGA3E1X7R1C105K080AC</td>
<td>TDK Corporation</td>
</tr>
<tr>
<td>COUT1</td>
<td>10 μF</td>
<td>CGA4J3X7S1A106K125AB</td>
<td>TDK Corporation</td>
</tr>
<tr>
<td>CFB</td>
<td>33 pF</td>
<td>--</td>
<td>--</td>
</tr>
<tr>
<td>RFB1</td>
<td>84 kΩ</td>
<td>--</td>
<td>--</td>
</tr>
<tr>
<td>RFB2</td>
<td>16 kΩ</td>
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</tbody>
</table>

Figure 13 shows the actual board.

![Actual Board Image](image)
### 3. 2 Measurement condition 2

Figure 14 shows a circuit diagram of S-19933C Evaluation Board. The parts listed in **Table 3** are mounted.

S-19933C (400 kHz), $V_{IN} = 13 \text{ V}$, $V_{OUT} = 5 \text{ V}$, $I_{OUT} = 600 \text{ mA}$,

Compliant with CISPR25 Edition 4.0 2016-10

---

**Table 3**

<table>
<thead>
<tr>
<th>Symbol</th>
<th>Value</th>
<th>Part Number</th>
<th>Manufacturer</th>
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</thead>
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<tr>
<td>$C_{F2}$</td>
<td>4.7 μF</td>
<td>CGA4J1X7R1H475K125AC</td>
<td>TDK Corporation</td>
</tr>
<tr>
<td>L2</td>
<td>4.7 μH</td>
<td>TFM252012ALVA4R7MTAA</td>
<td>TDK Corporation</td>
</tr>
<tr>
<td>$C_{F4}$</td>
<td>4.7 μF</td>
<td>CGA4J1X7R1H475K125AC</td>
<td>TDK Corporation</td>
</tr>
<tr>
<td>$C_{IN1}$</td>
<td>4.7 μF</td>
<td>CGA4J1X7R1H475K125AC</td>
<td>TDK Corporation</td>
</tr>
<tr>
<td>L1</td>
<td>33 μH</td>
<td>SPM6545VT-330M-D</td>
<td>TDK Corporation</td>
</tr>
<tr>
<td>$C_{REG1}$</td>
<td>1.0 μF</td>
<td>CGA3E1X7R1C105K080AC</td>
<td>TDK Corporation</td>
</tr>
<tr>
<td>$C_{OUT1}$</td>
<td>47 μF</td>
<td>CGA9N3X7R1C476M230KB</td>
<td>TDK Corporation</td>
</tr>
<tr>
<td>$C_{FB}$</td>
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<td>–</td>
<td>–</td>
</tr>
<tr>
<td>$R_{FB1}$</td>
<td>525 kΩ</td>
<td>–</td>
<td>–</td>
</tr>
<tr>
<td>$R_{FB2}$</td>
<td>100 kΩ</td>
<td>–</td>
<td>–</td>
</tr>
</tbody>
</table>

---

*1. Noise suppression parts

Figure 15 shows the actual board.
3.3 Measurement results of voltage method

Figure 16 and Figure 17 show measurement results of voltage method.

**S-19933A (2.2 MHz)**  Supply: VIN_EMI, Return: VSS_EMI, AV: average

![Figure 16](image)

**S-19933C (400 kHz)**  Supply: VIN_EMI, Return: VSS, AV: average

![Figure 17](image)
3. 4  Measurement results of ALSE method

Figure 18 to Figure 21 show measurement results of ALSE method.

S-19933A (2.2 MHz)  V: vertical, H: horizontal, AV: average

![Figure 18](image1)

![Figure 19](image2)
S-19933C (400 kHz)  V: vertical, H: horizontal, AV: average

Figure 20

Figure 21
4. Precautions

- The usages described in this application note are typical examples using ICs of ABLIC Inc. Perform thorough evaluation before use.

- Do not apply an electrostatic discharge to this IC that exceeds the performance ratings of the built-in electrostatic protection circuit.

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5. Related Sources

Refer to the following datasheets for details of the S-19932/19933 Series.

- S-19932A/19932B/19933A/19933B Series Datasheet
- S-19932C/19932D/19933C/19933D Series Datasheet

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